

Reverse Iodine Transfer Polymerization (RITP) in Emulsion

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Summary: Reverse iodine transfer polymerization (RITP) is a new controlled radical polymerization technique based on the use of molecular iodine I_2 as control agent. This paper aims at presenting the basics of RITP and the strategy that we have followed for the development of this process in the past three years, from the validation in homogeneous solution polymerization up to recent results in heterogeneous aqueous polymerization processes. Typical examples of RITP of butyl acrylate in emulsion and RITP of styrene in miniemulsion are discussed.

Keywords: emulsion polymerization; miniemulsion polymerization; reverse iodine transfer polymerization

Introduction

The area of radical polymerization has seen a real breakthrough with the invention of controlled/“living” radical polymerization techniques (CRP).^[1] These techniques make it possible to design copolymers with unusual chain microstructures (e.g. gradient copolymers, well-defined graft copolymers), copolymers of complex architectures that were only accessible by other specific methods such as living ionic polymerizations (e.g. block copolymers, star polymers, ...), copolymers with functional groups (e.g. homo- or hetero-telechelic polymers, macromonomers, functional star polymers, ...), and composites (e.g. polymer brushes from modified surfaces). The CRP techniques rely on a reversible activation-deactivation of the polymer chains, i.e. an equilibrium between a reservoir of dormant chains (capped polymer chains) and a tiny population of active chains (propagating chains) (Figure 1). Two main strategies have been used so far: the first one deals

with a reversible termination mechanism and the quality of the control is then essentially based on the persistent radical effect (i.e. an accumulation of the persistent species $[X-(Y)] \gg [P\bullet]$ leading to a favored cross-coupling rather than self-termination $R_c = k_c [X-(Y)][P\bullet] \gg R_t = k_t [P\bullet]^2$), the second one deals with a reversible chain transfer mechanism and the quality of the control is then essentially based on the high probability of reversible transfer reactions in comparison with termination (i.e. domination of degenerative chain transfer $R_{ex} = k_{ex} [P\bullet][P-X(+Y)] \gg R_t = k_t [P\bullet]^2$).^[2] Sometimes, the two processes (reversible termination and reversible transfer) can operate simultaneously (example: living radical polymerizations mediated by organocobalt porphyrin complexes reported by Wayland et al.^[3,4]). Several CRP techniques have been developed in the past thirty years, but their implementation at an industrial scale, especially in heterogeneous aqueous processes which are of major importance nowadays, remains a challenge.^[5,6] In this paper, we report our strategy to set up a new CRP technique based on simple, readily available and economical chemicals and our attempts to control the polymerization in aqueous emulsion polymerizations. Experimental details are given elsewhere.^[7–11]

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Table 1.Reverse iodine transfer polymerization in solution, emulsion and miniemulsion.^{a)}

Run	Solvent	Monomer	Additive	Time (h)	Conv. (%)	$M_{n,th}^{b)}$ ($g \cdot mol^{-1}$)	$M_{n,SEC}$ ($g \cdot mol^{-1}$)	M_w/M_n	pH	$d_p^{c)}$ (nm)
1	Butyl acetate	Butyl acrylate	No	5	95	9 500	9 700	1.83	n.a.	n.a. ^{d)}
2	Water (emulsion)	Butyl acrylate	No	7	99	10 300	31 000	1.98	5.2	106
3	Water (emulsion) (surfactant-free)	Butyl acrylate	No	15	83	8 700	22 000	1.88	5.1	443
4	Water (miniemulsion)	Styrene	No	16	72	7 500	13 900	1.73	2.4	334
5	Water (miniemulsion)	Styrene	H ₂ O ₂ /HCl	16	78	7 900	7 900	1.46	3.4	316

^{a)} Run 1: polymerization of *n*-butyl acrylate at 80% w/v versus butyl acetate as solvent ([BuA] = 3.30 M) in the presence of 2,2'-azobisisobutyronitrile as initiator with [AIBN]/[I₂] = 1.9, *T* = 85 °C. Run 2: polymerization of BuA in emulsion at *T* = 85 °C ([ACPA]/[I₂] = 1.7, [SDS] = 0.15 × CMC, $M_{n,targeted}$ = 10 400 $g \cdot mol^{-1}$). Run 3: polymerization of BuA in emulsion at *T* = 85 °C ([ACPA]/[I₂] = 1.6, no SDS, $M_{n,targeted}$ = 10 100 $g \cdot mol^{-1}$). Run 4: polymerization of styrene in miniemulsion at *T* = 60 °C in the presence of Perkadox 16S as initiator, [Perkadox]/[I₂] = 1.99. Run 5: polymerization of styrene in miniemulsion at *T* = 60 °C in the presence of Perkadox 16S as initiator, [Perkadox]/[I₂] = 2.44. BuA: *n*-butyl acrylate; ACPA: 4,4'-azobis(4-cyanopentanoic acid); AIBN: 2,2'-azobisisobutyronitrile; SDS: sodium dodecyl sulfate; CMC: critical micelle concentration; Perkadox 16S: bis(4-tert-butylcyclohexyl) peroxydicarbonate.

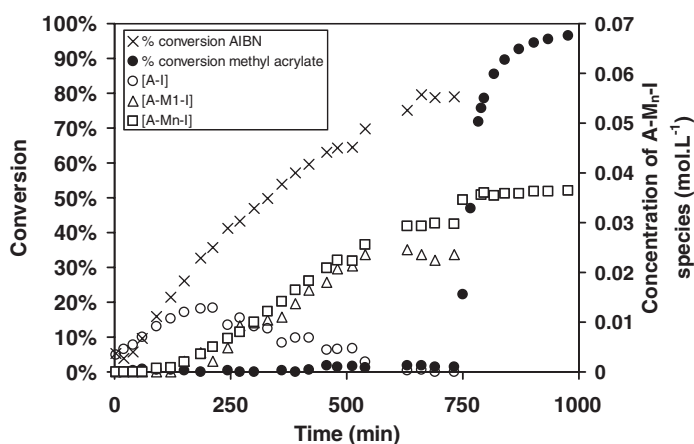
^{b)} Calculated by $M_{n,theoretical} = (\text{mass of monomer}) \times \text{Conversion} / (2 \times (\text{moles of } I_2)) + M_{A-1}$ in which M_{A-1} is the molecular weight of the chain ends.

^{c)} Particle diameter.

^{d)} Not applicable.

The kinetic analysis in the case of RITP of methyl acrylate at 70 °C showed the existence of an initialization period during which iodine is consumed to form short A-M_n-I telomers which can further act as reversible transfer agents (reversible chain

transfer) (Figure 3). For high monomer to iodine [M]/[I₂] ratio, the monomer conversion during this period is negligible: this is the reason why in most cases this period can be called “inhibition period” or “induction period”. This favored reaction of radicals

**Figure 3.**

Typical evolution of monomer conversion, initiator conversion, and concentrations of A-M_n-I species in reverse iodine transfer polymerization of methyl acrylate at 70 °C in deuterated benzene (determined by ¹H-NMR analyses) ([methyl acrylate] = 5.47 M, [C₆D₆] = 5.70 M, [2,2'-azobis(isobutyronitrile)] = 3.78 × 10⁻² M, and [I₂] = 2.22 × 10⁻² M).

with iodine is due to the high reactivity of iodine.^[23,24] Indeed, the scavenging of alkyl radicals by iodine I_2 is nearly a diffusion-controlled reaction (typically in the range 10^9 – $10^{10} \text{ M}^{-1} \cdot \text{s}^{-1}$) and it was reported that there are certainly no spin effects in the scavenging of alkyl radicals by iodine and that steric effects can be expected to be small.^[24] Furthermore, iodine radicals $I\bullet$ produced by the scavenging reaction can recombine to form I_2 and this reaction is again a very fast nearly diffusion-controlled reaction (in the range 10^9 – $10^{10} \text{ M}^{-1} \cdot \text{s}^{-1}$).^[24,25] Actually, the observed rate constants for the scavenging of alkyl radicals by iodine $R\bullet + I_2$ and for the recombination of iodine radicals $I\bullet + I\bullet$ were not found to be completely proportional to the inverse of the viscosity of the media, indicating that they are not solely diffusion rate-controlled, but they could be described with a combination of a diffusion-controlled rate constant and an activation-controlled rate constant.^[24]

After the induction period, the polymerization takes place and is dominated by the degenerative chain transfer mechanism. A typical evolution of the molecular weight and polydispersity index with conversion is given in Figure 4 in the case of RITP of

methyl methacrylate in toluene.^[8] The experimental data are in relatively good agreement with the theoretical evolutions of the molecular weight M_n (Eq. 1) and polydispersity index PDI (Eq. 2).^[12]

$$M_n = (p[M]_0 M_{\text{monomer}}) / \{2[I_2]_0 \times [1 - (1 - p)^{C_{\text{ex}}}] \} \quad (1)$$

$$PDI = \{1 + ([M]_0 / (2[I_2]_0)) \times [2 + (2 - p)(1 - C_{\text{ex}}) / C_{\text{ex}}] / \{p[M]_0 / (2[I_2]_0 [1 - (1 - p)^{C_{\text{ex}}}] \} \} \quad (2)$$

in which p is the fractional monomer conversion, M_{monomer} is the molecular weight of the monomer, $[I_2]_0$ is the initial concentration of iodine, and C_{ex} is the degenerative chain transfer constant.

In the case of poly(methyl acrylate) where the polymers chain-ends are stable enough to survive during a Maldi-Tof analysis (in addition to $^1\text{H-NMR}$, $^{13}\text{C-NMR}$, and SEC characterizations), the expected structure A- M_n -I was confirmed, supporting the proposed mechanism of RITP.^[7]

Ab Initio Emulsion Polymerization

Ab initio emulsion polymerization is one of the most used heterogeneous processes in

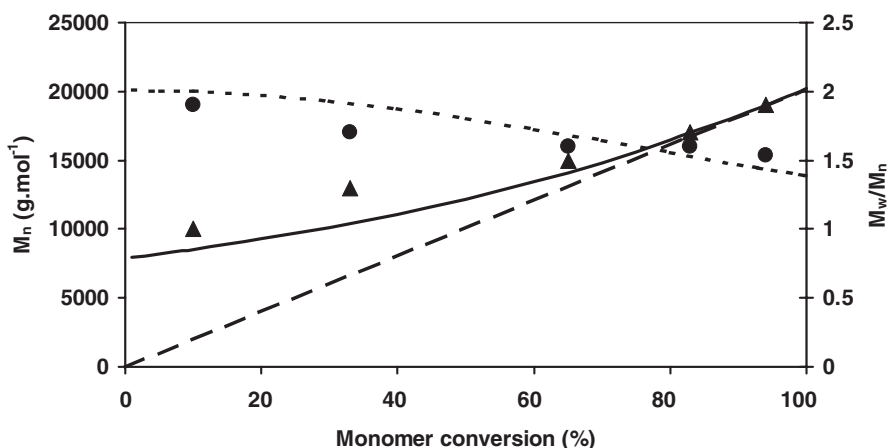


Figure 4.

Evolution of molecular weight M_n (▲) and polydispersity index M_w/M_n (●) with monomer conversion in reverse iodine transfer polymerization of methyl methacrylate in toluene at 80 °C in the presence of AIBN as initiator with $[AIBN]/[I_2] = 1.7$ ($M_{n,\text{targeted}} = 20\,200 \text{ g} \cdot \text{mol}^{-1}$). Theoretical evolutions are given by Eq. 1 (—) and Eq. 2 (---) with $C_{\text{ex}} = 2.6$. The ideal behavior of M_n assuming a high C_{ex} is also given for comparison (---).

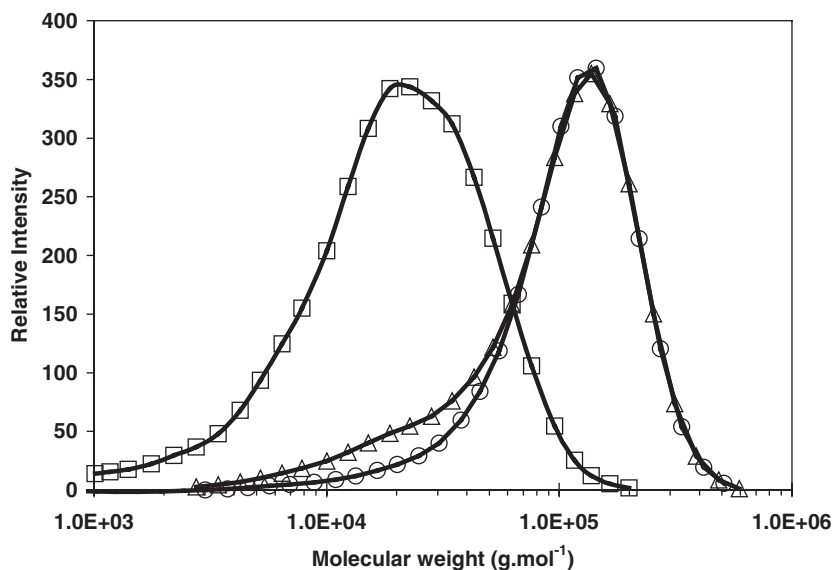


Figure 5.

Molecular weight distributions of the seed poly(BuA) latex ($M_{n,SEC} = 15\,900\text{ g} \cdot \text{mol}^{-1}$) prepared by RITP and of the block copolymer latex poly(butyl acrylate)-*b*-poly(styrene-*co*-butyl acrylate) ($M_{n,SEC} = 53\,400\text{ g} \cdot \text{mol}^{-1}$) prepared by seeded emulsion polymerization at 85°C : (\square) refractive index detector (seed latex), (\circ) UV detector at 254 nm (copolymer latex), (\triangle) refractive index detector (copolymer latex). Seed: $[\text{ACPA}]/[\text{I}_2] = 1.6$, $[\text{SDS}] = 0.15 \times \text{CMC}$, targeted $M_n = 2\,500\text{ g} \cdot \text{mol}^{-1}$, conversion = 40%, particle diameter = 127 nm; Block copolymer: second monomer = styrene; $\text{Monomer}_{\text{Feed}}/\text{Monomer}_{\text{Seed}} = 4.7\text{ w/w}$, conversion = 32%, particle diameter = 203 nm.

the industry.^[26] It initially involves two phases: a monomer phase dispersed in an aqueous phase containing a hydrosoluble radical initiator and a surfactant. The polymerization creates a new phase of polymer particles (nucleation). The nucleation step is very important since it will determine the number of particles (and so the final latex particle size) which in turn will partly determine the kinetics of the polymerization.^[27] Most CRP techniques tested so far failed in *ab initio* emulsion polymerization

because they encountered difficulties related to the nucleation step (e.g. instability of the latex, slow diffusion of hydrophobic control agents,...)^[5,6,28] and only a few works gave promising results.^[29] In our first attempts, we tested *ab initio* emulsion RITP of *n*-butyl acrylate, using 4,4'-azobis(4-cyanopentanoic acid) (ACPA) neutralized with sodium hydroxide as initiator and sodium dodecyl sulfate (SDS) as surfactant.^[9] It was possible to obtain a stable and uncolored (white) monodisperse

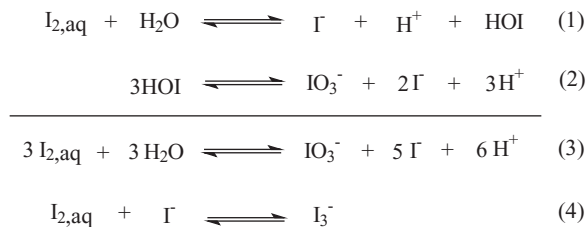
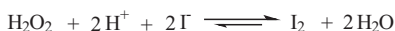


Figure 6.

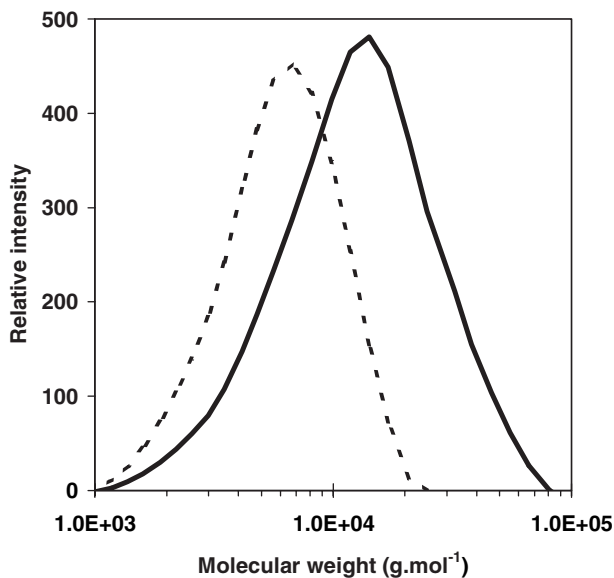
Some important reactions of iodine I_2 in the aqueous phase: hydrolytic disproportionation of iodine I_2 and triiodide I_3^- formation.

**Figure 7.**

Oxydation of iodide by hydrogen peroxide.

latex with high monomer conversion (Table 1, run 2). The potentially surface-active iodinated transfer agents synthesized in situ during the process (A-M_n-I oligomers in which A is a hydrophilic moiety from the radical initiator) can take part in the nucleation step and contribute to the electrostatic stabilization of the latex, as indicated by a successful surfactant-free RITP experiment in emulsion (Table 1, run 3). It was checked that the molecular weight of the latex could be tuned by varying the initial concentration of iodine [I₂]. Furthermore, the successful preparation of a block copolymer latex poly(butyl acrylate)-block-poly(styrene-co-butyl acrylate)

proved that the polymer chains could be reactivated (living character) (Figure 5). Nevertheless, it was also noticed that the molecular weights of the latexes prepared by RITP were much higher than the theoretical values, as shown in Table 1 runs 2-3. In order to account for this upward deviation of the molecular weights, the peculiarities of emulsion polymerization (partitioning of the reactants between the different phases) and the chemistry of iodine in water must be considered (Figure 6).^[10] Indeed, although the partitioning of iodine is in favor of the butyl acrylate monomer phase ($K = [\text{I}_2]_{\text{aq}}/[\text{I}_2]_{\text{BuA}} = 2.03 \times 10^{-3}$ at 25 °C), the disproportionation of iodine in water plays a serious deleterious role in the control of the polymerization. By following the evolution of the concentration of iodide [I⁻] by a selective electrode for the experiment of Table 1 run 2, it was shown that the side reaction of hydrolysis

**Figure 8.**

Molecular weight distributions of the seed polystyrene latex prepared by reverse iodine transfer polymerization in miniemulsion ($M_{n,SEC} = 4900 \text{ g} \cdot \text{mol}^{-1}$, $M_w/M_n = 1.48$, $M_{n,th} = 4100 \text{ g} \cdot \text{mol}^{-1}$, - - -) and the final polystyrene latex prepared by iodine transfer polymerization of styrene in seeded emulsion polymerization ($M_{n,SEC} = 8900 \text{ g} \cdot \text{mol}^{-1}$, $M_{n,th} = 9800 \text{ g} \cdot \text{mol}^{-1}$, —). Seed latex (miniemulsion polymerization at $T = 60^\circ\text{C}$): water (150 g), I₂ (0.3833 g, 1.51 mmol), n-hexadecane (0.45 g, 1.99 mmol), styrene (15 g, 144 mmol), Perkadox 165 (1.495 g, 3.75 mmol), dodecyl sulfate sodium salt (0.4 g, 1.39 mmol) and addition of hydrogen peroxide (0.7 g H₂O₂ 30% wt. solution in water, 6.23 mmol) in 15 g of water during 3 hours; Chain extension (seeded emulsion polymerization at 75 °C): seed PS-I latex (42.5 g, $M_n = 4900 \text{ g} \cdot \text{mol}^{-1}$, 0.54 mmol), α,α' -azobisisobutyronitrile (0.0233 g, 0.142 mmol), styrene (3.01 g, 28.9 mmol).

was actually very important and that only 33% of the initial iodine was effectively consumed through the RITP mechanism ($\alpha = n_{I_2, \text{effective}}/n_{I_2, \text{initial}} = 33\%$). Based on this value of 33%, the experimental molecular weight now matches the corrected targeted value ($M_{n, \text{targeted (corrected)}} = (\text{mass of monomer}) / (2 \times \alpha \times n_{I_2, \text{initial}}) + M_{A-I} = 31\,000 \text{ g} \cdot \text{mol}^{-1}$). The identification of the side reactions was a key step toward the development of improved RITP procedures in heterogeneous aqueous processes as described below.

Miniemulsion Polymerization

In order to counterbalance the hydrolytic disproportionation of iodine in water, a modified RITP procedure was developed. The new procedure is based on the use of an oxidant to regenerate iodine I_2 by oxidation of iodide I^- . In this section, this new concept is illustrated in the case of miniemulsion polymerization of styrene by RITP initiated by bis(4-tert-butylcyclohexyl) peroxydicarbonate (Perkadox 16S) at $T = 60^\circ\text{C}$ with dodecyl sulfate sodium salt as surfactant and hexadecane as hydrophobe.^[11] The continuous addition of hydrogen peroxide (as oxidant) in acidic conditions leads to the oxidation of iodide I^- to form iodine I_2 and water (Figure 7). This new concept allowed us to prepare a stable polystyrene latex with a much better agreement between theoretical and experimental molecular weight (Table 1, run 5) than the corresponding RITP in the absence of hydrogen peroxide (Table 1, run 4). Furthermore, the successful chain-extension (resuming the polymerization with a new shot of styrene and AIBN) indicates that the living character of the RITP polymerization is maintained with this new procedure (Figure 8).

Conclusion

The RITP process has been invented few years ago and it has rapidly led to promising results in heterogeneous aqueous processes. Stable and uncolored (white) monodisperse poly(butyl acrylate) latex could be

obtained by RITP in emulsion. However, a large deviation of the molecular weights from the theoretical values was observed in the early attempts of RITP in emulsion: hydrolytic disproportionation of iodine has been identified as a serious deleterious side reaction. Based on this knowledge, an improved RITP procedure has been set up that is based on the use of an oxidant to regenerate iodine. For instance, RITP of styrene in miniemulsion has been successfully performed with a continuous addition of hydrogen peroxide as oxidant. Thanks to this new concept, in addition to the living character of the latex, a good correlation between theoretical and experimental molecular weights can now be obtained, reinforcing the interest of RITP for the industrial development of controlled radical polymerization in dispersed aqueous processes. Our current efforts focus on the application of this new concept to a wide range of experimental conditions to test its robustness.

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